

On Page 31, Paragraph 4:

---

The spot diameter  $\phi_1$  on focussing is given by

2

$$\begin{aligned} & (S_{pp}/2) \times 2 \times (\beta_A \times \beta_2)^2 \times \{(2 \cdot NA)/(\beta_A \times \beta_2)\} \\ & = 2 \cdot NA \cdot S_{pp} \cdot (\beta_A \times \beta_2) \end{aligned}$$

...(1).

---

On Page 32, Paragraph 1:

---

If, in the above equation 1, the focussing pull-in range  $S_p$  is fixed and the spot diameter  $\phi_1$  on focussing is fixed, the spot diameter  $\phi_1$  is given by

$$\phi = 2 \cdot NA \cdot S_{pp} \cdot (\beta_A \times \beta_2) = \text{constant}$$

so that the multiplication factor  $\beta_2$  for the direction 2 for detecting the tracking error and the land-groove discrimination signal is in proportion to  $1/\beta_A$ .

3

$$\beta_2 \propto 1/\beta_A$$

So, the variation of the spot diameter  $\phi_2$  for the defocussing  $\Delta_{def}$  is

A

$$\Delta\phi_2/\Delta_{Def} = 4 \cdot NA \cdot \beta_2 \propto 1/\beta_A$$

...(3)

so that it is inversely proportional to the multiplication factor  $\beta_A$  of the anamorphic prism. Meanwhile, if the direction of the multiplication factor of the anamorphic prism is the radial direction, it suffices to substitute  $1/\beta_A$  for  $\beta_A$ .

---

### REMARKS

This preliminary amendment is filed to correct the specification. If the Examiner has any suggestions for placing this application in even better form, the Examiner is invited to telephone